



# Hydrodynamic performance of psammosteids: New insights from computational fluid dynamics simulations

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**The shape of dermal armor protecting the body in the Paleozoic agnathans such as the Heterostaci has an important hydrodynamic role in providing lift or drag force generation. Here, by performing computational fluid dynamics simulations (CFD), the measurements of hydrodynamic lift/drag force and lift or drag coefficients were taken for two psammosteids *Guerichosteus* and *Tartuosteus* with reference to the pteraspid *Errivaspis*. This study shows the substantially higher values of the lift coefficient and lift-to-drag ratio for the psammosteids *Guerichosteus* and *Tartuosteus* compared with *Errivaspis*. The tendencies in the evolution of dermal exoskeleton, especially the widening of the branchial plates of psammosteids was directed towards the increased generation of lift force to provide efficient cruising.**

## Introduction

The Heterostraci are a Silurian–Devonian clade of jawless vertebrates characterized by a pair of common external branchial openings. The two major groups are Cyathaspidiformes and Pteraspidiformes and are represented by a large variety of forms (e.g., Blicek 1984; Denison 1964; Janvier 1996). Cyathaspidiformes possess a head shield that is oval to almost circular in cross section, an adaptation believed to be related to producing lift force for a rapid rise from the bottom (Novitskaya 2007). *Pteraspis*, in turn, also have oval cross-sections of a head shield but are wider laterally. Conversely, the head shield of psammosteids are dorso-ventral asymmetric with wide branchial plates (Obruchev and Mark-Kurik 1965; Tarlo 1964, 1965), which are purportedly more efficient at creating lift.

The fish body shape is significantly connected to functional aspects of hydrodynamic, locomotion, and their swimming mode (Aleyev 1977; Webb 1984). Therefore the study of these aspects on Recent fishes offers the tools for the partial reconstruction of the mode of life and habits of fossil fishes. Recently, the hydrodynamics of the cephalic shield of *Errivaspis* was studied in a wind tunnel to show the detailed flow pattern around the head shield which was shown to be comparable with a delta wing aircraft (Botella and Farina 2008).

The purpose of this article is to investigate the hydrodynamic effects of the psammosteid body plan, a poorly understood feature of psammosteid morphology. Psammosteids are considered to be bottom-dwellers (Tarlo 1957). Some authors

suggested that they fed on starfish which they picked up from the sea floor (Patten 1932), but they have also been interpreted as mud grubbers living in shallow seas (Tarlo 1965). The wide and downwardly curved branchial plates of large psammosteids were considered to be a support while resting on soft bottom substrates (Janvier 1996). In addition to the supporting nature of the head shield, the tail fin of the psammosteid *Drepanaspis gemuendenensis*, which comprises the 1/4 of the total length of the body, is responsible for generating considerable propulsive force (Mark-Kurik 1992). These fishes, regardless of their possible substrate-dwelling habits, were also capable of active swimming.

A new reconstruction of *Guerichosteus kozlowskii* recently shed light on the body shape of this psammosteids (Dec 2019). The development of computer methods that use numerical analysis and data structures to solve and analyze problems that involve fluid flows (computational fluid mechanics) gives the possibility of a better understanding of the hydrodynamic properties (Rahman 2017) of the psammosteid body form.

Assessing the drag and lift forces, generated on hydrofoils is an important step in identifying the performance characteristic of the hydrofoil during swimming. This study focusses on the psammosteid gliding locomotion, especially the influence of the geometrical shape of the psammosteid body form on hydrodynamic performance. In this instance, gliding involves the motionless movement of the body through a current and represents the steady state condition of flow over the body surface.

**Abbreviations.**—A, surface wetted area [m<sup>2</sup>];  $\alpha$ , angle of attack; C<sub>D</sub>, drag coefficient; C<sub>L</sub>, lift coefficient; C<sub>L</sub>/C<sub>D</sub>, lift-to-drag ratio; CFD, computational fluid dynamics; D, drag forces [N]; L, lift forces [N]; N, Newtons; p, pressure [Pa];  $\rho$ , density of fluid; Re, Reynolds number; U, velocity [ms<sup>-1</sup>];  $\nu$ , kinematic viscosity [m<sup>2</sup>s<sup>-1</sup>].

## Methods

The computer used for the simulation is a Linux Ubuntu 18.10 machine running on a Intel® Core™ i7-2630QM CPU 2.00GHz × 8 with 16GB RAM.

**Mesh generation.**—A 3D model of *Errivaspis* and *Guerichosteus* (Fig. 1) was created using the free and open-source 3D computer graphics software Blender. The model of *Errivaspis*

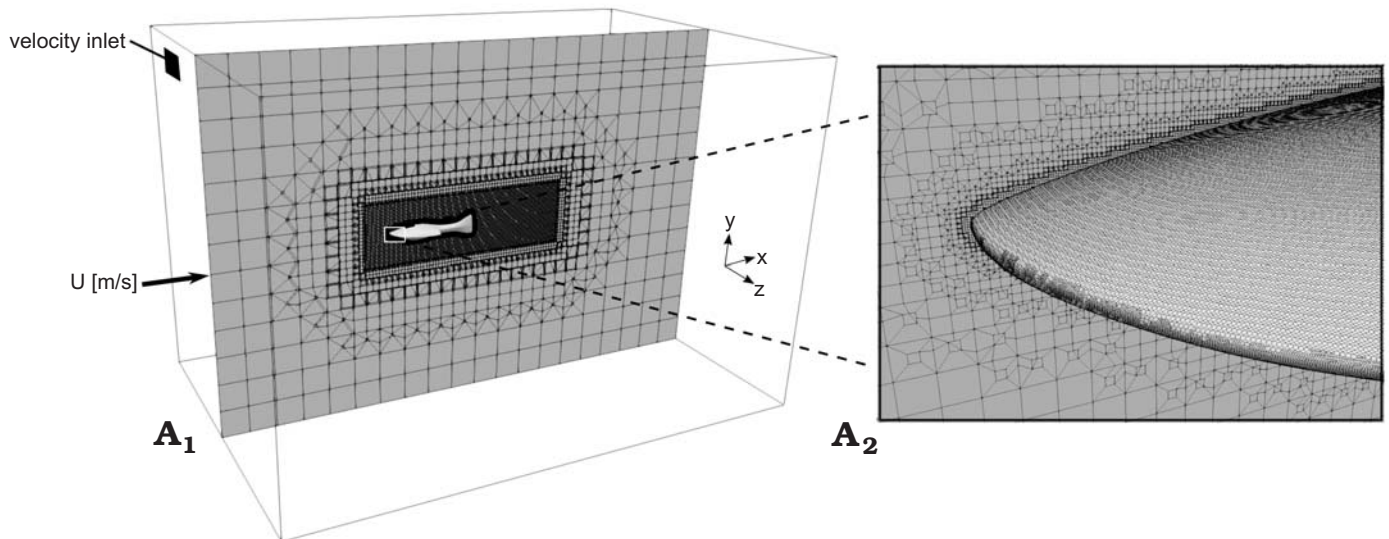


Fig. 1. Box-shaped flow domain, mesh and coordinate system used for computational fluid dynamics (A<sub>1</sub>); A<sub>2</sub>, enlargement view on the mesh.

was created based on Botella and Farina (2008). Only the tail was modified where the extended lower lobe was shortened (Mark-Kurik and Botella 2009). The *Guerichosteus* mesh was created in reference to work by Dec (2019) concerning the revision and 3D reconstruction of the genus. To compare the geometry characteristics of the 3D models, all models were scaled to the same length (0.5 m). The triangulated surface geometries were exported from Blender as .stl files to the snappyHexMesh tool (OpenFoam). A computational box-shaped flow domain with width and height of 2 m and a length of 3 m was generated (Fig. 1A<sub>1</sub>) (Moukalled et al. 2016). To increase mesh fineness around the fish models a refinement volume region (1.18 m in length, 0.38 m in width and height) was set. The cells (with additional cells layer near surface) are mostly located in the region around the model which allows for a good resolution of the wake region (Moukalled et al. 2016). The mesh statistics are shown in Table 1 and details of the grid generated around the model are shown in Fig. 1A<sub>2</sub>.

**Boundary and initial condition.**—The range of Reynolds numbers conducted in simulation varies from 238 000 to 1 190 000, using the equation  $Re = Ul/\nu$ , where  $U$  is the flow speed ( $\text{ms}^{-1}$ ),  $l$  is the length of the object in the direction of flow, in this case the chord length (0.5 m),  $\nu$  refers to the kinematic viscosity (sea water =  $1.05\text{e-}6 \text{ m}^2\text{s}^{-1}$ ). The simulation consists of flow around a fish model at various angles of attack ( $\alpha$ ) and velocity. The

Table 1. The mesh statistics.

	<i>Errivaspis</i>	<i>Guerichostes</i>	<i>Tartuosteus</i>
Area [ $\text{m}^2$ ]	0.100157	0.158854	0.192262
Number of cells	1 549 095	2 351 444	2 871 719
Number of surface cells	277 381	449 677	524 244
Average surface face area [ $\text{m}^2$ ]	3.61e-07	3.53e-07	3.67e-07
Minimum surface face area [ $\text{m}^2$ ]	2.34e-09	2.65e-09	1.28e-09

angle of attack converging a range from -10 to +20 degrees in two degree increments.

The boundary face was defined as the velocity inlet with various speed ( $0.5 \text{ ms}^{-1}$ ,  $1.5 \text{ ms}^{-1}$ ,  $2.5 \text{ ms}^{-1}$ ) in different cases. In analogy to the previous analysis of *Errivaspis* the swimming speed was estimated for three body length per second (Botella and Farina 2008). Here for the model of 0.5 m long, the swimming speed of three body length per second gives the value of velocity  $1.5 \text{ ms}^{-1}$ . The top speed of five body length per second (here  $2.5 \text{ ms}^{-1}$ ) is applied in reference to the boxfish (Van Wassenbergh et al. 2014). This fish has a carapace protecting the body so undulation to power swimming is limited to rare. Therefore, like psammosetids are believed to have swum, the acceleration is a result of the single beats of the caudal fin.

The front, back, upper and lower walls were set to slip boundary condition to provide a slip constraint. For the simulation of turbulent flows the Reynolds-Averaged Simulation (RAS) model was applied with komegaSST turbulent modeling. The simpleFoam steady-state solver for incompressible, turbulent flow was used in the open-source package OpenFoam. This solver uses the SIMPLE algorithm which is an iterative process that is repeated until convergence. In most cases iterative convergence was reached after 500 iterations. The simulation result is the sum of the forces acting in each direction on the model, or any part of it. The lift and drag force were calculated in Paraview software by summing up the pressure distribution around the whole model surface.

Lift force is defined as the component of the net force (due to viscous and pressure forces) that is perpendicular (along Y axis) to the flow direction (along X axis). Drag force is the component of the net force along the flow direction (along X axis), that is opposed to the motion. So the lift and drag force of the model is the vector sum of the pressure times the area around the entire solid body.

The lift or drag coefficient has been applied to eliminate the size effect as a universally comparable measure of lift/drag force. The lift and drag coefficient is a number used to model

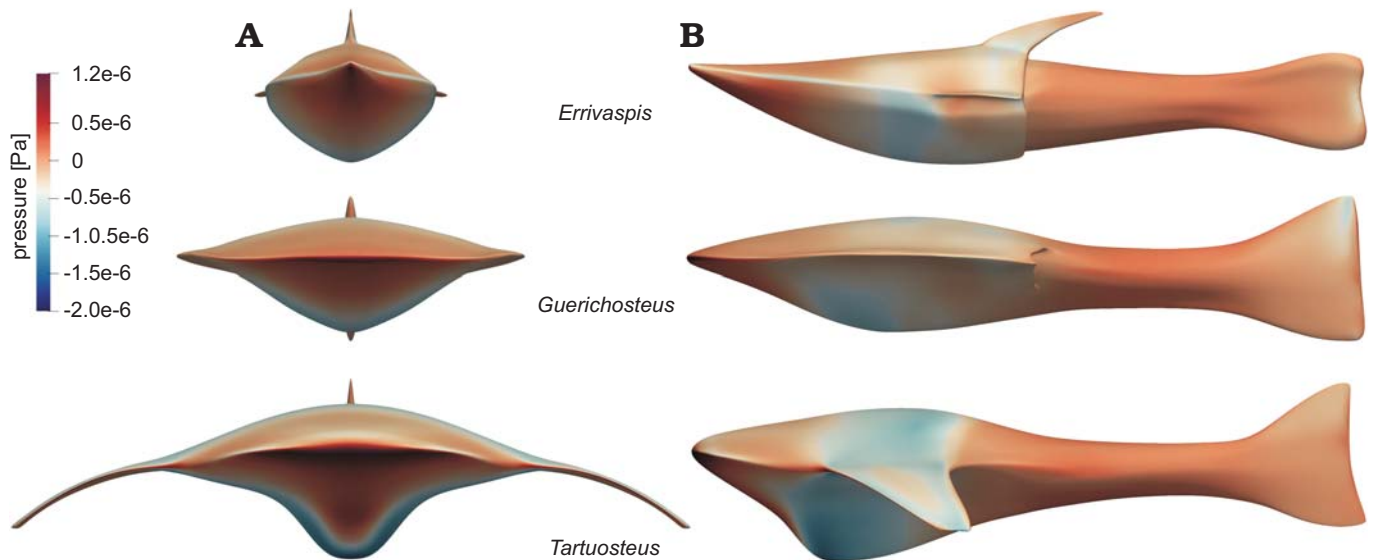


Fig. 2. Distribution of pressure on the fish bodies at flow velocity  $1.5 \text{ ms}^{-1}$ , in anterior ( $A_1$ ) and lateral ( $A_2$ ) views.

all of the complex dependencies of shape (size and body shape), inclination, and some flow conditions (velocity, viscosity).

The lift coefficient  $C_L = 2L/\rho U^2 A$ .

The drag coefficient  $C_D = 2D/\rho U^2 A$ .

## Results

**Pressure.**—The surface pressure distribution on the fish models at  $1.5 \text{ ms}^{-1}$  velocity is presented on Fig. 2. Defined gauge pressure is the pressure relative to 0 Pa set in simulation boundary condition. Gauge pressure is positive for pressures above boundary condition pressure, and negative for pressures below it.

In each models, the highest pressures are registered in the anterior part of the head and at the leading edges of the branchial plates in the case of *Tartuosteus*. The lowest pressures are observed in the middle and thickest part of the head shield. The area of low pressure extends around the mid part of the body, including branchial plates, of *Tartuosteus*. While in *Guerichosteus* and *Errivaspis* it is mainly observed in the ventral plate.

**Lift.**—The variation of lift coefficient with angle of attack and various flow speeds are shown in Fig. 3A. The lift coefficient increases near linearly with the angle of attack  $\alpha$  for each tested flow velocity for all three models. Only for *Tartuosteus*  $C_L$  reaches a maximum at about  $8^\circ$ , and then starts to decrease. This decrease of lift is called stall and it is generated by flow separation. It is not observed for two other models due to a limited range of analysis and it will occur at high angles of attack.

**Drag.**—The most efficient model for generating lift, indicated by body orientation, also exhibits the lowest drag (Fig. 3B). The lowest drag observed in all three genera is between  $-4^\circ$  and  $0^\circ$   $\alpha$  for  $0.5 \text{ ms}^{-1}$  and  $1.5 \text{ ms}^{-1}$  velocity and rapidly increased with increasing angle of attack. At a velocity of  $2.5 \text{ ms}^{-1}$  the drag coefficient  $C_D$  shows a similar pattern to the drag force for *Errivaspis*, whereas for *Guerichosteus* ( $\alpha -6^\circ$  to  $-4^\circ$ ) and

*Tartuosteus* ( $\alpha -4^\circ$  to  $-2^\circ$ ) a narrower range of degree of the lowest  $C_D$  was found than in *Errivaspis*.

The minimum drag coefficient at  $0.5 \text{ ms}^{-1}$  flow velocity for the three genera can be ordered as: *Errivaspis* ( $C_D = 0.0037$ ) < *Guerichosteus* ( $C_D = 0.0065$ ) < *Tartuosteus* ( $C_D = 0.0101$ ). In all models the drag coefficient decreased with increasing velocity. So when flow velocities increased to  $2.5 \text{ ms}^{-1}$ , the minimum  $C_D$  for *Errivaspis* decreased as well ( $C_D = 0.0025$ ). This value is smaller than for the other two genera *Guerichosteus* and *Tartuosteus*, where drag coefficient values are almost the same ( $C_D = 0.0033$ ) at  $2.5 \text{ ms}^{-1}$ .

The tip vortex associated with induced drag is generated by the branchial plate tip, similar to an airplane wing (see Çengel and Cimbala 2006: fig. 10-49, 10-50). The produced vortices reduce the pressure along the rear edge of the branchial plate, increasing drag. The vorticity shown in Fig. 4 is presented with the iso-vorticity surface at  $U = 1.5 \text{ ms}^{-1}$  and  $\alpha = 0^\circ$  and identified by Q-criterion (Kolář 2007). The most abundant vortex is observed in *Tartuosteus* and *Guerichosteus*, and is considerably less in *Errivaspis*. However, through analogy from modern aircraft, the further a trailing vortex is from the body of the branchial plates, the less influence on the plate (Çengel and Cimbala 2006). Therefore *Tartuosteus* long branchial plates produce less drag produced by vortex drag than *Guerichosteus*, but reduce maneuverability because of their larger moment of inertia.

**Lift-to-drag ratio.**—The ratio is a measure of hydrodynamic performance for the fish model, which is equivalent to the ratio of the lift-to-drag coefficients  $C_L/C_D$ . This is shown in Fig. 3C in a plot of  $C_L/C_D$  versus the angle of attack with various speed ( $0.5 \text{ ms}^{-1}$ ,  $1.5 \text{ ms}^{-1}$ ,  $2.5 \text{ ms}^{-1}$ ).

The lift-to-drag ratio of three genera increases with the angle of attack  $\alpha$ . At a velocity of  $0.5 \text{ ms}^{-1}$  it reaches a maximum at  $\alpha = 4^\circ$  for *Tartuosteus*,  $\alpha = 6^\circ$  for *Errivaspis* and *Guerichosteus*. For the three genera, the maximum  $C_L/C_D$  of  $0.5 \text{ ms}^{-1}$  flow velocity is ordered: *Errivaspis* ( $C_L/C_D = 4.13$ ) < *Guerichosteus* ( $C_L/C_D = 6.56$ ) < *Tartuosteus* ( $C_L/C_D = 8.29$ ). In a higher flow

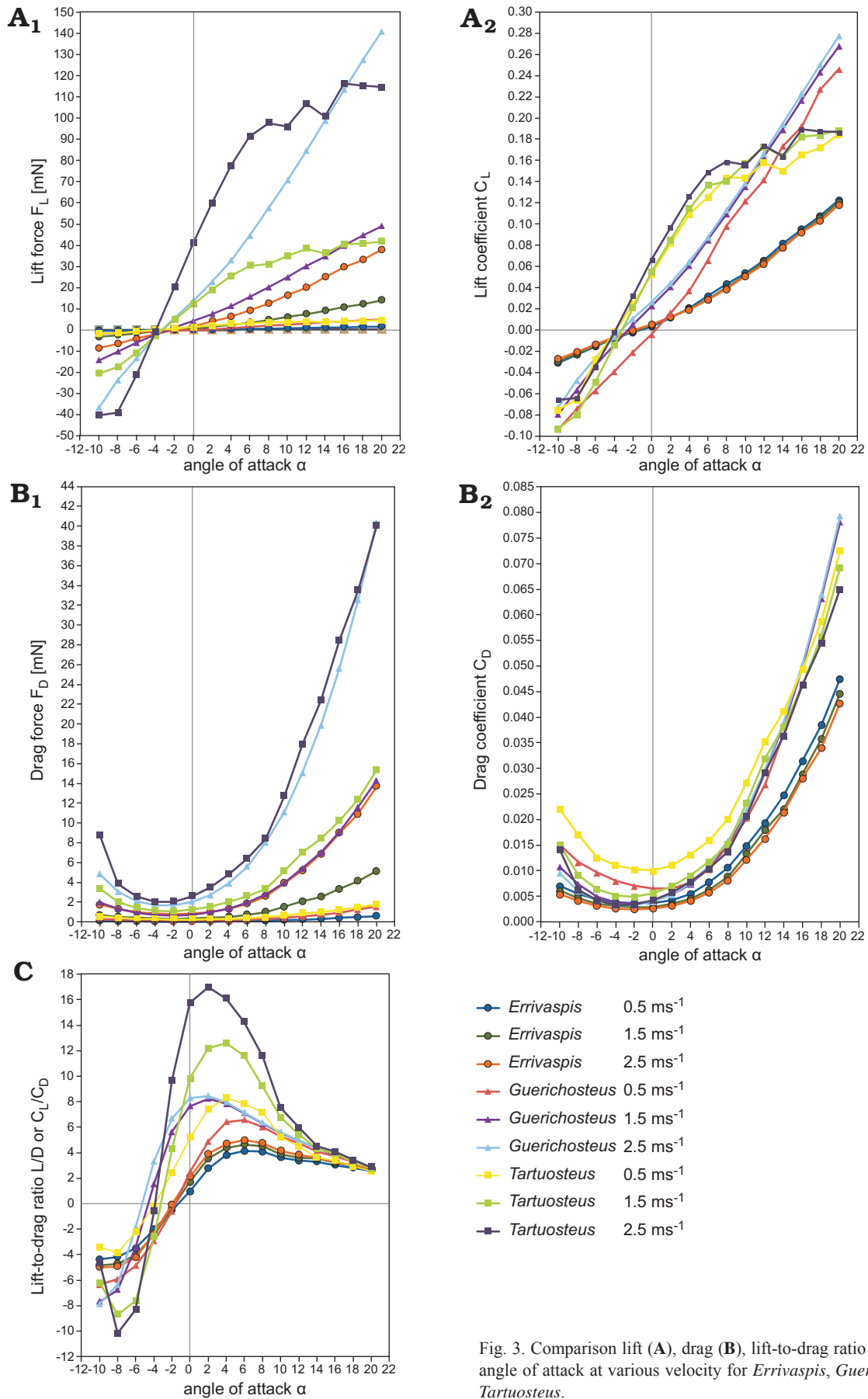


Fig. 3. Comparison lift (A), drag (B), lift-to-drag ratio (C) versus the angle of attack at various velocity for *Errivaspis*, *Guerichosteus*, and *Tartuosteus*.

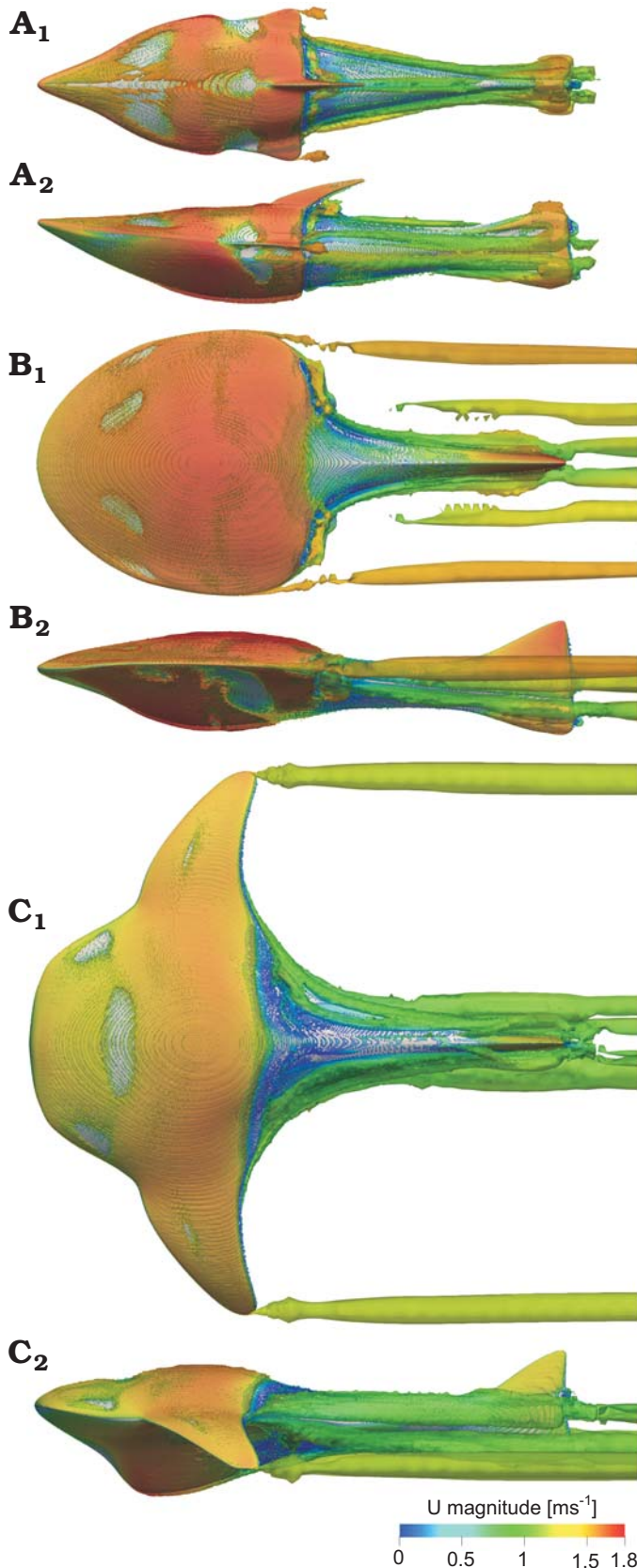


Fig. 4. Vorticity patterns using Q-criterion for 0 angles of attack and flow velocity  $1.5 \text{ ms}^{-1}$  in *Errivaspis* (A), *Guerichosteus* (B), and *Tartuosteus* (C). Models displayed in left lateral ( $A_1$ – $C_1$ ) and top ( $A_2$ – $C_2$ ) views. Iso-vorticity surface is colored by the magnitude of velocity.

velocity of  $2.5 \text{ ms}^{-1}$  the lift-to-drag ratio differs from the lower velocities and the maximum  $C_L/C_D$  is at  $\alpha = 2^\circ$  for *Tartuosteus* and *Guerichosteus* and  $\alpha = 6^\circ$  for *Errivaspis*. In *Tartuosteus* the lift-to-drag ratio at  $2.5 \text{ ms}^{-1}$  flow velocity increased twice to 16.99 compared to  $0.5 \text{ ms}^{-1}$ , while for *Errivaspis* it raised only to 4.98 and for *Guerichosteus* to 8.46.

### Concluding remarks

CFD simulation was performed to investigate the hydrodynamic properties (qualitative and quantitative) of gliding psammosteids, *Guerichosteus* (Early Devonian) and *Tartuosteus* (Middle Devonian). The properties of their body armor differ mostly in the proportions of the branchial plates, which are broader in *Tartuosteus* (Obruchev and Mark-Kurik 1965) than in *Guerichosteus* (Dec 2019), and is critical for hydrodynamic efficiency, where the main propulsive power is generated by the tail. CFD simulation of the three agnathan genera has been performed to verify the hypothesis that the broadening of the branchial plate increased the lift force generation to provide efficient cruising.

Changing the angle of attack has been shown to result in a change of lift and drag. The more streamlined body produces a lower drag coefficient, and for the three genera studied, *Errivaspis* has the lowest drag coefficients at varying current velocities followed *Guerichosteus* then *Tartuosteus*. The drag coefficient is comparable to living animals, for example dolphins, in which the drag coefficient on the wetted skin area is about 0.0035 (Çengel and Cimbala 2006). Producing the least drag and generating the most lift are desirable characteristics of swimming organisms that need to maintain a depth in the water column. The change of the lift and drag characteristics of models is related to the changes of the angles of attack. The most favorable lift-to drag ratio (positive values) at higher velocities of  $2.5 \text{ ms}^{-1}$  was experienced by *Tartuosteus*. *Guerichosteus* and *Errivaspis* exhibited similar lift-to drag ratios at the same velocity. To produce more lift, the angle of attack has to be higher, however, the maximum  $C_L/C_D$  is noted in lower angles of attack for *Tartuosteus* and *Guerichosteus* than for *Errivaspis*. The highest lift-to-drag ratio is noted for *Tartuosteus* ( $C_L/C_D = 16.99$ ) which is comparable to jet airplane (Airbus A320-200  $C_L/C_D = 16.3$ ; Martinez-Val et al. 2005).

This study demonstrates the adaptive reason behind the relative widening of branchial plates in psammosteids. The widening of branchial plates increases the lift force, which apparently provide efficient cruising. Additionally, the wider branchial plates of *Tartuosteus* might have reduced its maneuverability, comparing to *Guerichosteus* and *Errivaspis*.

Higher hydrodynamic quality suggests advantages of *Tartuosteus* in more effective acquisition of widely distributed food or for predator escape. However, the ecomorphologic classification is still ambiguous, there is not enough information of the ecological connection of psammosteids with the bottom (benthonekton) or with the water column (planktonekton, eunekton).

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